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# Influence of the Rear Interface on Composition and Photoluminescence Yield of CZTSSe Absorbers: A Case for an Al<sub>2</sub>O<sub>3</sub> **Intermediate Layer**

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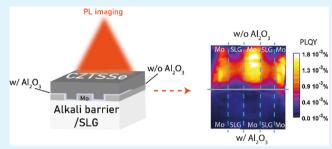
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ABSTRACT: The rear interface of kesterite absorbers with Mo back contact represents one of the possible sources of nonradiative voltage losses ( $\Delta V_{\text{oc,nrad}}$ ) because of the reported decomposition reactions, an uncontrolled growth of MoSe2, or a nonoptimal electrical contact with high recombination. Several intermediate layers (IL), such as MoO<sub>3</sub>, TiN, and ZnO, have been tested to mitigate these issues, and efficiency improvements have been reported. However, the introduction of IL also triggers other effects such as changes in alkali diffusion, altered morphology, and modifications in the absorber composition, all factors that can also influence  $\Delta V_{
m oc,nrad}$ . In this study, the different effects are decoupled



by designing a special sample that directly compares four rear structures (SLG, SLG/Mo, SLG/Al<sub>2</sub>O<sub>3</sub>, and SLG/Mo/Al<sub>2</sub>O<sub>3</sub>) with a Na-doped kesterite absorber optimized for a device efficiency >10%. The IL of choice is Al<sub>2</sub>O<sub>3</sub> because of its reported beneficial effect to reduce the surface recombination velocity at the rear interface of solar cell absorbers. Identical annealing conditions and alkali distribution in the kesterite absorber are preserved, as measured by time-of-flight secondary ion mass spectrometry and energydispersive X-ray spectroscopy. The lowest  $\Delta V_{
m oc,nrad}$  of 290 mV is measured for kesterite grown on Mo, whereas the kesterite absorber on Al<sub>2</sub>O<sub>3</sub> exhibits higher nonradiative losses up to 350 mV. The anticipated field-effect passivation from Al<sub>2</sub>O<sub>3</sub> at the rear interface could not be observed for the kesterite absorbers prepared by the two-step process, further confirmed by an additional experiment with air annealing. Our results suggest that Mo with an in situ formed MoSe<sub>2</sub> remains a suitable back contact for high-efficiency kesterite devices.

KEYWORDS: kesterite, CZTSSe, solar cell, back contact, photoluminescence, Al<sub>2</sub>O<sub>3</sub>, nonradiative recombination

## 1. INTRODUCTION

The best kesterite solar cell devices of many laboratories around the world 1-4 are approaching the world record efficiency of 12.6%, reached by IBM in 2013.5 Despite all the efforts in finely optimizing the crystallization process, the problem of high  $V_{\text{oc,SQ}}$  deficit (expressed as  $V_{\text{oc,SQ}} - V_{\text{oc}}$ , with  $V_{
m oc, SQ}$  defined by the Shockley-Queisser limit) remains unresolved. The introduction of alkali metals proved to boost PV characteristics, but the minimum  $V_{\text{oc,SQ}}$  deficit is still 0.29 V even for the best performing devices, 6,7 whereas for CIGS, it is below 0.15 V.8

Several studies suggest that the Mo back contact could be one of the factors limiting the  $V_{\rm oc}$ . A possible reason is the decomposition of kesterite when in contact with the Mo layer at high temperatures. Mo reacts with the chalcogen vapors forming a Mo(S,Se)<sub>2</sub> layer, the growth of which is difficult to control as it depends on multiple interrelated factors such as the Mo layer structure, duration, and temperature of the annealing process and chalcogen overpressure in the annealing chamber. Furthermore, it is still debated whether the  $Mo(S_1Se)_2/CZTSSe$  interface ensures an appropriate electrical contact.10

The addition of an intermediate layer (IL) between the kesterite absorber and Mo has been reported to reduce or avoid the formation of Mo(S,Se)<sub>2</sub> by limiting the diffusion of Se to the back. Table 1 presents a collection of representative studies on the implementation of various materials as IL. While the influence on the  $Mo(S,Se)_2$  growth varies, all papers report an increased efficiency relative to the baseline. So comes the

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Table 1. Comparison of Observed Influences (Change in MoSe, Thickness, Diffusion of Alkalis, and Other Additional Effects on Absorber Growth) Correlated with Introducing an IL between the Mo Layer and Kesterite Absorber from Recent **Publications** 

IL material/absorber type	efficiency improvement (%) <sup>a</sup>	Mo(S,Se) <sub>2</sub> thickness	alkalis diffusion <sup>b</sup>		additional effects	reference
MoO <sub>3</sub> (10 nm)/CZTS	+19	-	↓Na	↑K	improved crystallization	12
$MoO_3$ (-)/CZTS	+30	$\downarrow$	↑K		fewer voids at the back	13
TiN (200 nm)/CZTS(e) $^c$	+100	$\downarrow$	↑Na		improved crystallization	14
$Al_2O_3$ (3 nm)/CZTS	+10	$\downarrow$	↑Na		ZnS segregation from back to the surface	15
$TiB_2$ (30 nm)/CZTS	+42	$\downarrow$	-		smaller grains	16
ZnO (10 nm)/CZTSe	+140	-	-		bilayer formation + less secondary phases	17
a-SiC (10 nm)/CZTSe	+16	-	-		increased grain size	18

<sup>a</sup>Efficiency improvement relative to the baseline device presented in the reference. <sup>b</sup>An arrow pointing upward (downward) represents a measured increase (decrease) in the content of the indicated alkali metal in the kesterite absorber. Both CZTS and CZTSe absorbers have been tested. The presence of TiN is beneficial in both cases. The results in the table are for the CZTS absorber only.

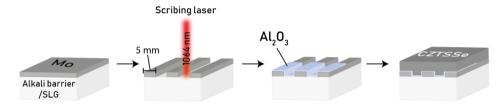


Figure 1. Process schematics to obtain the four rear structures (SLG/Mo, SLG/Mo/Al<sub>2</sub>O<sub>3</sub>, SLG, and SLG/Al<sub>2</sub>O<sub>3</sub>) with a single SLG substrate and a CZTSSe absorber.

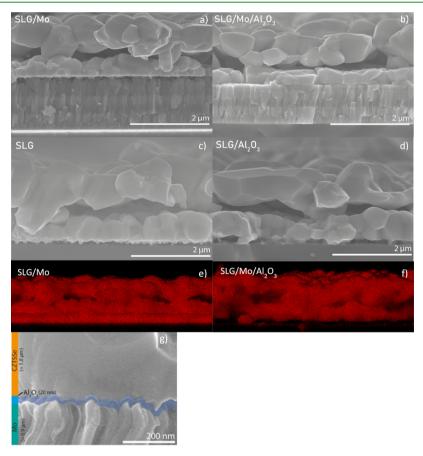


Figure 2. SEM cross-sectional images of the CZTSSe absorber on (a) SLG/Mo, (b) SLG/Mo/Al<sub>2</sub>O<sub>3</sub>, (c) bare SLG, and (d) SLG/Al<sub>2</sub>O<sub>3</sub>. (e), (f) SEM-EDS cross-sectional measurements for Se net counts for CZTSSe on SLG/Mo and SLG/Mo/Al<sub>2</sub>O<sub>3</sub> structures, respectively. (g) Highresolution SEM cross section of the CZTSSe absorber deposited on Al<sub>2</sub>O<sub>3</sub> on the Mo side. Al<sub>2</sub>O<sub>3</sub> is highlighted with the blue color for clarity.

question: is the increase in performance related to the influence of the IL on the Mo(S,Se)2 growth or on absorber

growth dynamics? The question is justified by the additional reported effects (shown in Table 1) the IL has on alkali diffusion from the glass substrate, crystallization dynamics, and phase segregation. Further uncertainty is caused by Mo surface roughness. A conformal deposition is necessary to ensure barrier properties against Se diffusion. 11 These interconnected issues make it challenging to fully understand the origin of the performance improvement and if controlling Mo(S,Se), thickness is beneficial.

In this study, a special sample design was considered to preserve the composition and annealing conditions of the absorber while allowing the comparison of four rear structures (Figure 1). The sample preparation can be divided into the following steps:

- 1 laser scribing of the Mo layer into 5 mm wide lines;
- 2 deposition of a conformal 20 nm thick Al<sub>2</sub>O<sub>3</sub> layer by atomic layer deposition (ALD) on half of the scribed Mo layer and the other half was covered to keep it Al<sub>2</sub>O<sub>3</sub>
- 3 spin-coating of a Na-doped CZTS precursor solution;
- 4 annealing in a rapid thermal processing (RTP) oven in a Se-rich atmosphere at temperatures up to 550 °C. We used the three-stage annealing profile process developed by Haass et al., 19 with which a device efficiency of up to 11% can be achieved.

The as-obtained sample allows for a direct comparison of a single CZTSSe absorber grown on four rear structures: SLG/ Mo, SLG/Mo/Al<sub>2</sub>O<sub>3</sub>, SLG, and SLG/Al<sub>2</sub>O<sub>3</sub>, corresponding to three different rear interfaces: Mo/CZTSSe, Al<sub>2</sub>O<sub>3</sub>/CZTSSe, and SLG/CZTSSe.

Al<sub>2</sub>O<sub>3</sub> was the IL of choice because it reduces surface recombination and increases charge carrier lifetime, thanks to the low defect density at the interface. 20 The presence of fixed negative charges (corresponding to aluminum vacancies and/ or oxygen interstitials) leads to upward band bending at the absorber interface, which repels the minority charge carriers. 21,22 This passivation effect is reported to be maximized after annealing treatments. 23,24

Successful implementation of  $Al_2O_3$  as a passivating layer has been reported for Si,  $^{23,25}$  CIGS,  $^{22,26-28}$  and CZTS  $^{28-31}$  solar cell devices, but in such cases, the Al<sub>2</sub>O<sub>3</sub> layer is typically patterned or thinner than 5 nm. This allows for carrier collection and absorber adhesion but limits the magnitude of the passivating effect.<sup>2</sup>

This study aims to clarify the influence of an IL at the rear interface on absorber growth and the  $V_{oc}$  of a single absorber. According to the literature, 23 the thickness of 20 nm of the Al<sub>2</sub>O<sub>3</sub> layer and the annealing temperatures up to 550 °C should provide the best passivation properties. The effectiveness of the passivation is investigated by extracting the nonradiative recombination losses ( $\Delta V_{\rm oc,nrad}$ ) from quantitative photoluminescence (PL) measurements.

# 2. RESULTS AND DISCUSSION

2.1. Morphology and Crystallinity. Figure 2 presents the SEM cross sections of the absorber on the four rear structures (SLG/Mo, SLG/Mo/Al<sub>2</sub>O<sub>3</sub>, SLG, and SLG/Al<sub>2</sub>O<sub>3</sub>). There is no noticeable difference in morphology or thickness (about  $1.7-2 \mu m$ ) among the cross sections, indicating that the growth dynamics of the absorber layer was comparable. The bare Mo layer reached a thickness of about 1.3  $\mu$ m after selenization due to  $Mo(S_1Se)_2$  formation. The Mo layer with  $Al_2O_3$  on top measures about 0.9  $\mu$ m (same as the as-deposited Mo layer), indicating that Al<sub>2</sub>O<sub>3</sub> is an effective barrier for Se

diffusion and that it withstands the annealing conditions. Figure 2g shows a high-resolution SEM cross section of the compact Al<sub>2</sub>O<sub>3</sub> layer sandwiched between a CZTSSe grain and the Mo layer.

X-ray diffraction (XRD) measurements were carried out with a pinhole of 0.5 mm in diameter attached to the primary beam to assess whether the rear structure affects the absorber crystallinity. Such a configuration allows focusing the X-ray beam on specific locations of the sample. Figure 3a shows the

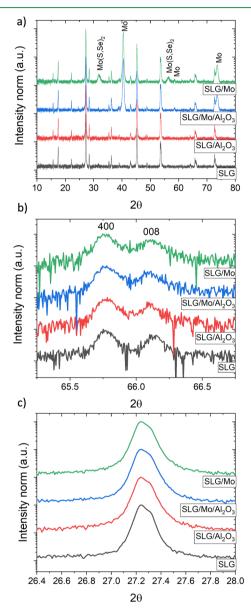


Figure 3. XRD patterns for the CZTSSe absorber grown on four different rear structures. (a) Full XRD pattern ( $10^{\circ} < 2\theta < 80^{\circ}$ ). (b) High-resolution XRD pattern (65° <  $2\theta$  < 67°) after stripping the Kα2 signal. (c) Zoomed 112 Bragg reflex.

full XRD pattern ( $10^{\circ} < 2\theta < 80^{\circ}$ ) measured on four sample areas, each corresponding to a different rear structure. Bragg reflexes at 17.47°, 27.23°, and 45.25° confirm the CZTSSe phase.<sup>32</sup> Mo(S,Se)<sub>2</sub> diffraction peaks (31.76° and 56.32°) appear only for the side with bare Mo. Thus,  $Mo(S,Se)_2$  is absent or too thin to be measured for the Mo/Al<sub>2</sub>O<sub>3</sub> structure. This result is further confirmed through scanning electron

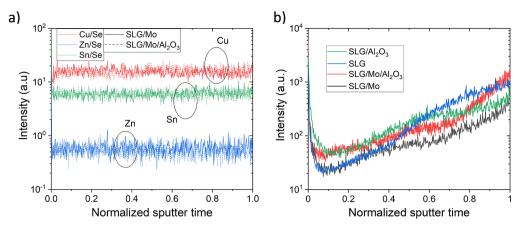


Figure 4. Normalized TOF-SIMS depth profiles of (a) Cu, Zn, and Sn for CZTSSe and SLG/Mo and SLG/Mo/ $Al_2O_3$ . (b) Comparison of normalized Na depth profiles for the CZTSSe absorber on the four structures SLG/Mo, SLG/Mo/ $Al_2O_3$ , SLG, and SLG/ $Al_2O_3$ .

microscopy and energy dispersive X-ray spectroscopy (SEM-EDS) Se maps of the cross sections for SLG/Mo/CZTSSe and SLG/Mo/Al<sub>2</sub>O<sub>3</sub>/CZTSSe structures (Figure 2e,f, respectively), where a Se-rich layer is visible beneath the CZTSSe absorber only for the SLG/Mo/CZTSSe structure. The 400-008 Bragg kesterite diffractions (Figure 3b), which represent lattice parameters a and c, respectively, are aligned among the four measurements, indicating a similar order/disorder of the Cu/Zn sublattice. 33,34 The primary 112 Bragg kesterite diffraction is positioned at 27.23° (Figure 3c) for each part of the absorber and indicates a S/(S + Se) ratio of about 5%, as calculated with Vegard's law.<sup>35</sup> Additional microprobe analysis of an absorber with a comparable composition measured a S content of 2.7 at. % and Se of 48.1 at.%, which corresponds to a S/(S + Se) ratio of 5%. The full width at half-maximum (FWHM) for the 112 diffraction peak among the three rear structures (SLG/Mo, SLG/Mo/Al<sub>2</sub>O<sub>3</sub>, and SLG/Al<sub>2</sub>O<sub>3</sub>) is  $0.137 \pm 0.003$ , whereas for bare glass, it is  $0.127 \pm 0.003$ . For other samples with the same composition, we measured the FWHM in the range of 0.194-0.247 and did not see any correlation with the rear structure. Therefore, the small difference measured for the sample in this manuscript is insignificant and within statistical error. Eventually, no secondary phases can be identified, although the presence of Zn(S,Se) and Cu<sub>2</sub>Sn(S,Se)<sub>3</sub> impurity phases cannot be excluded since their Bragg reflexes coincide with those of CZTSSe and therefore cannot be distinguished by XRD.<sup>36</sup>

2.2. Composition. Time-of-flight secondary ion mass spectrometry (TOF-SIMS) allows investigating the elemental depth profiles qualitatively. In Figure 4, both the signal intensity of the matrix elements (Cu, Zn, and Sn) and the sputtering time are normalized, the first by the Se signal intensity and the latter by the absorber depth. The reported profile comparison between CZTSSe on SLG/Mo and SLG/ Mo/Al<sub>2</sub>O<sub>3</sub> structures is representative of all the measurements. The flat profiles of the matrix elements Cu, Zn, and Sn indicate that the presence or absence of Mo and/or Al<sub>2</sub>O<sub>3</sub> does not influence the composition of the absorber throughout its thickness. The result is confirmed by EDS maps (Figure S5), where matrix elements (Cu, Zn, and Sn) are homogeneously distributed within the absorber thickness. The depth profile in Figure S4 for the CZTSSe absorber on the rear structure SLG/ Mo/Al<sub>2</sub>O<sub>3</sub> reveals the Al signal in the expected area between Mo and the absorber. One cannot rule out the presence of an unintentional Al doping in the CZTSSe absorber beyond the

resolution of the SIMS measurement; however, small amounts of Al should not be harmful, but rather beneficial to electrical properties.<sup>37</sup> As indicated in Table 1, the addition of an IL can influence alkali-metal diffusion, with Na playing a significant role in affecting morphological and electrical characteristics of kesterite absorbers.  $^{38-40}$  In this study, an  $SiO_x$  alkali barrier was sputtered before Mo deposition. This does not entirely block the Na out-diffusion from the SLG substrate but allows to control it. External Na doping is employed, in the form of NaCl added to the kesterite precursor solution, to provide a homogeneous Na source. A stronger Na signal at the absorber interfaces (Figure 4b) is expected and already observed in other studies. The signal peak at the front might be explained by Na evaporation from the SLG during the annealing and its subsequent condensation on the front surface of the absorber. In contrast, an increase in Na intensity toward the back of the absorber is due to Na diffusion from the SLG. 38,41,42 No systematic difference in the Na shape profile correlated with the rear structure can be observed. As measured by EDS, the Na concentration amounts to about  $1 \pm 0.4$  at.% for each part of the sample (Figure S2d), thus confirming conclusions from TOF-SIMS measurements of a comparable Na concentration in the bulk of the absorber layer.

X-ray photoelectron spectroscopy (XPS) measurements were carried out to investigate chemical modifications of the surface (Figure S1). As observed in other studies, a thin oxide layer forms on the surface due to exposure to an ambient atmosphere, while the matrix elements exhibit similar depth profiles. <sup>43</sup>

A qualitative assessment of the metal ratios for the absorber bulk was obtained through X-ray fluorescence (XRF) mapping, which allows for detecting changes at a finer resolution than TOF-SIMS. In Figure 5, a correlation of Zn/Sn and Cu/Sn

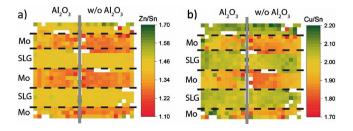


Figure 5. (a) Zn/Sn and (b) Cu/Sn XRF metal ratio maps.

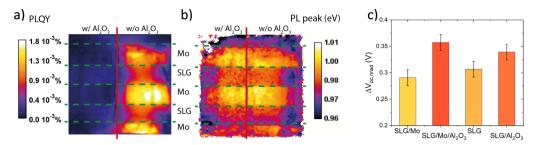


Figure 6. (a) Map of the PLQY. (b) Map of the PL peak position. (c) Conversion of PLQY intensity in nonradiative losses ( $\Delta V_{\text{oc,nrad}}$ ).

metal ratios in the presence or absence of the Mo layer can be observed. In contrast, the presence of  $\mathrm{Al_2O_3}$  does not cause any noticeable influence on the composition. Areas without Mo have a Zn-richer and Sn-poorer composition compared to the areas with Mo. The heat reflection from metals like Mo can lead to lower temperatures during annealing than the areas without Mo, leading to increased reevaporation of Sn in the latter ones. The XRF fitting reliability was assessed by comparing the results with SEM-EDS measurements of a similarly processed sample (see Figure S2).

The material characterization presented so far demonstrates that the absorber growth was equivalent concerning morphology and the Na content comparable among the four sample areas corresponding to the four rear structures. Small variations in metal ratios were detected between Mo and Mo-free areas, whereas the ratios were identical for  ${\rm Al_2O_3}$ - and  ${\rm Al_2O_3}$ -free areas.

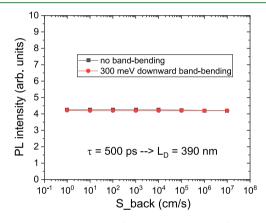
**2.3.** Nonradiative Recombination Losses ( $\Delta V_{\rm oc,nrad}$ ). 2.3.1. PL from the Front of the Absorber. Quantitative PL (also known as absolute PL or photoluminescence quantum yield, PLQY) allows calculating the nonradiative voltage losses following the formula  $\Delta V_{\rm oc,nrad} = -kT \ln(\text{PLQY})$ , where PLQY is the measured calibrated PL intensity. The PLQY measurement was carried out with an excitation laser wavelength of 660 nm.

A color-coded PL image is presented in Figure 6a, where brighter areas imply a stronger PLQY intensity, thus reduced nonradiative voltage losses compared to the darker areas. Nonradiative voltage loss ( $\Delta V_{\rm oc,nrad}$ ) values are presented in Figure 6c. Figure 6b shows a color-coded map for the PL peak position, where color brightness is proportional to the PL peak.

Starting with the side without Al<sub>2</sub>O<sub>3</sub> (right side of the sample in Figure 6a), one can compare CZTSSe grown on SLG and SLG/Mo. The kesterite grown on Mo has a brighter PLQY signal amounting to nonradiative voltage losses of about 290 mV, roughly 10-15 mV lower than on SLG. For reference, comparable losses were measured for Li-doped CZTSSe solar cell devices delivering an efficiency higher than 10%.2 The PL peak position shifts comparably to the  $\Delta V_{
m oc,nrad}$  difference between areas with or without Mo (Figure 6b). The PL emission of CZTSSe grown on Mo peaks at roughly 1 eV, about 10-15 meV higher than CZTSSe on areas without Mo. The peak shift agrees with the Sn content variation observed with XRF measurements in Figure 5, as similarly reported in previous studies.  $^{45,46}$  By comparison, such a  $V_{oc}$  variation is within the experimental statistical error for the solutionprocessed kesterite in our laboratory.

However, the side with  $Al_2O_3$  (left side of the sample) has the highest  $\Delta V_{\rm oc,nrad}$  losses of the sample, which amount to about 350 mV, regardless of the presence or absence of Mo

beneath  $Al_2O_3$ . The result is surprising for two main reasons: the influence of the rear structures (SLG or SLG/ $Al_2O_3$ ) and interface ( $Al_2O_3/CZTSSe$ ) on the PL measured from the front should not be so pronounced for an absorber with a thickness of about 2  $\mu$ m. Simulations of the PL intensity in function of the recombination velocity at the rear interface were carried out with a solar cell capacitance simulator (SCAPS) (see Figure 7) to evaluate the extent to which the rear interface can



**Figure 7.** SCAPS simulation of the PL intensity in function of the recombination velocity at the back interface in the case of no band bending at the back and a downward band bending of 300 meV.

influence the PL measurement from the front surface. We used the following set of parameters to model the absorber: an absorber thickness of 2  $\mu$ m, band gap of 1 eV, minority charge mobility  $\mu=120~{\rm cm^2/V},^{47}$  and a lifetime  $\tau=500~{\rm ps},^{48}$  which leads to a diffusion length of the minority charge carrier  $L_{\rm D}<0.5~\mu$ m based on the formula  $L_{\rm D}=(\tau\mu k_{\rm B}T/q)^{0.5}$ . Considering the surprising negative effect of the Al<sub>2</sub>O<sub>3</sub> layer on PL, two hypothetical worst-case scenarios where the bands are not bending upward as expected were examined: one where Al<sub>2</sub>O<sub>3</sub> does not create any band bending and the other with an arbitrary 300 meV downward band bending at the back. It can be observed that the PL intensity does not depend on the recombination velocity at the rear interface for both scenarios.

There is no measurable difference in composition and Na distribution between the CZTSSe absorber grown on  $Al_2O_3$  (left side) and the one grown without (right side), which could justify the increased nonradiative losses. The result indicates that the presence of the  $Al_2O_3$  IL must have additional effects that were not considered and cannot be assessed within the resolution of the absorber characterization techniques.

2.3.2. PL from the Back of the Absorber. The transparency of the SLG substrate allows carrying out PLQY measurements on the back of the sample on areas where Mo is not present. In

this manner, the passivation of  $Al_2O_3$  is directly assessed through the PL signal intensity. In this case, the analysis will be qualitative and the  $\Delta V_{\rm oc,nrad}$  will not be extracted since the system for the PLQY measurement is not calibrated for recording photon emissions through a layer of glass.

Figure 8 shows the PL map recorded from the back of the sample. It can be noticed that in this case, the intensity of the

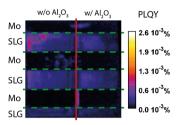


Figure 8. Map of the PLOY, as recorded through the SLG substrate.

PL between CZTSSe on SLG and  $SLG/Al_2O_3$  rear structures is comparable. It follows that the presence of  $Al_2O_3$  is not contributing to reducing the nonradiative recombination.

Considering the cross sections presented in Figure 1, one might suggest that the grainy morphology hinders the passivation or limits the absorption of the material. To rule out this factor, a Li-doped CZTSSe absorber displaying a compact morphology with large grains was considered (see Figure 3a for the cross section) and compared with the Nadoped absorber. The PL intensity measured from the back (Figure S3c) is of the same order of magnitude between the two samples. Thus, we can conclude that the morphological compactness did not influence the PL intensity or the contact quality with the  $\mathrm{Al}_2\mathrm{O}_3$  layer.

**2.4.** Investigation of the Al<sub>2</sub>O<sub>3</sub> Layer in an MOS Structure. To further understand the lacking passivation effect of the Al<sub>2</sub>O<sub>3</sub>, a metal-oxide semiconductor (MOS) structure, where the layer structure is SLG/Mo/CZTSSe/

Al $_2O_3$  with e-beam evaporated Ni–Al contacts, was fabricated (schematic in Figure 9a). This type of device structure allows for a qualitative investigation of the CZTSSe/Al $_2O_3$  interface by capacitance—voltage (CV) measurements. Two MOS samples were prepared: one was measured after the Al $_2O_3$  deposition (AD = as deposited). The other was heated on a hot plate at 350 °C in air for 5 min after Al $_2O_3$  deposition (PDA = postdeposition annealing). The PDA is carried out at a temperature that is as close as possible to the annealing temperature used to crystallize CZTSSe absorbers, <sup>49</sup> so as to mimic its effect on the CZTSSe/Al $_2O_3$  interface, while avoiding absorber decomposition. <sup>50,51</sup>

For both devices, the capacitance was measured in forward and reverse bias in a voltage range of -2 to 2 V at 1 kHz (Figure 9b). Larger voltages caused the breakdown of the dielectric (Al<sub>2</sub>O<sub>3</sub>). The capacitance drops at a negative voltage for the AD device, indicating a negative flat band voltage. This correlates with the presence of net positive fixed charges in the Al<sub>2</sub>O<sub>3</sub> layer; thus, the Al<sub>2</sub>O<sub>3</sub> layer in the AD device is oxygendeficient or aluminum-rich. 22 It would follow a downward band bending at the interface with the CZTSSe absorber, contrary to what is required for repelling the minority charge carriers. Kotipalli et al.<sup>24</sup> observed a similar behavior for the same type of device structure but with a CIGS absorber. The negative net fixed charges were recovered after an annealing procedure in a Se-rich atmosphere at T > 500 °C. At such a temperature, kesterite absorbers decompose;<sup>52</sup> thus, a similar annealing procedure was not considered for this study.

For the PDA device, no capacitance drop can be measured within the voltage range of the analysis. This entails that the fixed charges in the Al<sub>2</sub>O<sub>3</sub> layer are neutralized or that their influence cannot be measured within the chosen voltage range. For a qualitative assessment of the charge profile, TOF-SIMS measurements were performed on the two MOS devices (Figure 9c). A significant influence can be observed for the oxygen profile throughout the Al<sub>2</sub>O<sub>3</sub> layer depth. The PDA device presents a noticeably lower intensity for O<sup>-</sup> ions, while

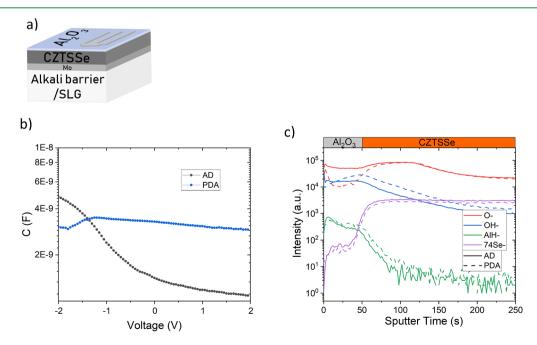


Figure 9. (a) Schematic of the MOS structure  $SLG/Mo/CZTSSe/Al_2O_3$ . (b) CV measurement at room-temperature of MOS devices with the  $Al_2O_3$  as-deposited (AD) on Mo and after heating on a hotplate (PDA). (c) TOF-SIMS measurements of MOS devices for negative ions.

the intensity for the  $OH^-$  ions increases correspondingly. This suggests hydrogen passivation of the dangling oxygen bonds, further reducing the amount of negative charges. Therefore, we can conclude that high-temperature annealing changes  $Al_2O_3$  composition, hence the amount of static charges, which shifts the flat band voltage to more negative values than -2 V. Eventually, this results in a lack of passivation at the CZTSSe interface, as is observed with the PL measurements in Figure 8.  $^{21}$ 

Our experiment was carried out on a kesterite absorber that was prepared with a two-stepmethod using a solution-processed precursor. There are many other methods for preparing the precursor including evaporation, sputtering, and spray-coating among others. As all of these approaches require a high-temperature crystallization step, we believe that our results are valid for kesterite absorbers obtained with the two-step method. <sup>49</sup> The effect, however, can also be dependent on the thickness of the  $\mathrm{Al}_2\mathrm{O}_3$ .

## 3. CONCLUSIONS

In this study, a single absorber was grown on four rear structures (SLG/Mo, SLG/Mo/Al<sub>2</sub>O<sub>3</sub>, SLG, and SLG/Al<sub>2</sub>O<sub>3</sub>), allowing the testing of the influence of the rear interfaces and presence of Mo on the absorber composition and nonradiative voltage losses, as extracted from the PLQY. Small variations in the composition could be observed between areas with or without the Mo layer, but not with the Al<sub>2</sub>O<sub>3</sub> IL, while the Na distribution and quantity in the bulk and on the surface are comparable among all absorber parts.

From PL measurements on both the front and the back interfaces of the absorber, we observed the following:

For front PL: the part of the CZTSSe absorber with  $Al_2O_3$  at the back has higher nonradiative losses than the part without it. The cause of the increased losses could not be identified with the resolution of the characterization techniques considered in the present study.

For back PL measured through the SLG substrate: the  $Al_2O_3$  layer does not provide a measurable passivation effect. This can be explained by a net amount of positive fixed charges in the  $Al_2O_3$  layer appearing after the kesterite precursor deposition.

Eventually, this study enabled us to verify that different rear structures can influence the absorber metal ratios, despite an unchanged morphology. While the IL  ${\rm Al_2O_3}$  limits the diffusion of Se to the back and avoids the contact of kesterite with the Mo layer, this does not lead to any positive impact on the  $\Delta V_{\rm oc,nrad}$  of an absorber optimized for a device efficiency >10%. This is explained by a negative influence of the two-step fabrication procedure necessary for kesterite absorbers on the passivating properties of the  ${\rm Al_2O_3}$  layer. The results further indicate that the Mo back contact represents the best solution for kesterite absorbers, and the reduction in  $\Delta V_{\rm oc,nrad}$  should be addressed by identifying and passivating the detrimental defects present in the kesterite bulk material.

## 4. EXPERIMENTAL SECTION

- **4.1. Chemicals.** The precursor solution consisted of thiourea (99%+, Sigma-Aldrich), tin chloride dihydrate ( $SnCl_2 \cdot _2H_2O$ , 98%, Sigma-Aldrich), zinc chloride ( $ZnCl_2$ , 99.99%, Alfa Aesar), copper chloride dihydrate ( $CuCl_2 \cdot 2H_2O$ ,  $\geq$ 99.99%, Sigma-Aldrich), and sodium chloride (NaCl, 99.99%, Alfa Aesar) dissolved in dimethyl sulfoxide (DMSO, 99.9%, Alfa Aesar).
- **4.2. Sample Preparation.** A 200–300 nm thick  $SiO_x$  alkali diffusion barrier layer was sputtered onto a 1 mm thick soda-lime glass

(SLG) with subsequent deposition of about 1  $\mu$ m molybdenum. The molybdenum layer was patterned with a picosecond pulse laser with a wavelength of 1064 nm, power of 750 mW, and frequency of 20 kHz. The Al<sub>2</sub>O<sub>3</sub> layer was deposited with a Fiji G2 ALD system (Veeco Instruments, Inc.). The process was performed at a substrate temperature of 150 °C with argon as a carrier gas at a base pressure of 25 Pa. The precursors were trimethylaluminum (TMA) (Sigma-Aldrich) and H2O. TMA and H2O were kept unheated. The growth rate was determined by ellipsometry on Si (100) reference substrates, and linear growth was observed with a growth rate of 0.99 Å cycle<sup>-1</sup>. The precursor solution was spin-coated onto the Mo layer and dried on a hotplate at 320 °C in air. The spin-coating and drying steps were repeated 12 times to obtain the desired precursor film thickness of about 1.7–2  $\mu$ m. All samples were annealed in an RTP furnace (RTP Annealsys AS ONE 150) inside a closed graphite box with selenium pellets (800 mg). The temperature gradient employed for annealing was the three-stage process holding at 300, 500, and 550 °C. 19 After selenization, the absorbers were immersed for 5 min in a 10 wt % (NH)<sub>4</sub>S<sub>2</sub> solution to clean the surface from contaminations and oxides.

4.3. Composition and Morphology. SEM measurements were performed using a Hitachi S-4800 electron microscope. EDS measurements were performed using a Zeiss 1550 SEM with the Oxford AZtec EDS system and an ESEM QuantaFEG650 from FEI (ThermoFisher) with detectors such as ETD (Everhart-Thornley detector) for SE imaging, CBS (concentric-backscattering detector) for BSE imaging, and EDX: ThermoNoran with SDD (Si-drift detector) 60 mm<sup>2</sup>. XPS measurements were performed using a Quantum2000 photoelectron spectrometer from Physical Electronics with a monochromatic Al Ka source, operated at a base pressure below 10<sup>-9</sup> mbar. XRF was performed with a Bruker M4 Tornado, using a rhodium tube operated at 20 keV as an X-ray source. A total of 625 data points (spot size  $\approx 20\mu m$  diameter) were acquired over the sample. The spectra were then evaluated with an SLG/Mo/MoSe<sub>2</sub>/ CZTSSe multilayer model (using the Bruker software suite), using elemental metals and chalcogen layers as calibration standards. Depth profile measurements were performed with a TOF-SIMS system from ION-TOF using O+2 primary ions with 2 keV of ion energy, a current of 400 nA, and a raster size of 300  $\times$  300  $\mu$ m<sup>2</sup>. An area of 100  $\times$  100  $\mu$ m<sup>2</sup> in-depth profiles was analyzed using Bi<sup>+</sup> ions with 25 keV of ion

Microprobe analysis was carried out with a JXA-8530F JEOL SUPERPROBE, equipped with a field emission electron probe microanalyzer (FE-EPMA) and four crystal spectrometers (WDS) in a  $3 \times 3 \text{ mm}^2$  square area on the center of the absorber layer.

- **4.4. Crystallinity.** XRD patterns for thin films were recorded in  $2\theta/\theta$  scan mode using a Bruker D8 diffractometer with Cu  $K\alpha$  radiation ( $\lambda = 1.5418$  Å, beam voltage: 40 kV, beam current: 40 mA, calibrated using Si(100) and Si(111) single crystals), a step size of  $0.05^{\circ}$ , and a scan rate of 0.5 s step<sup>-1</sup> for the full pattern and a step size of  $0.005^{\circ}$  and a scan rate of 2 s step<sup>-1</sup> for the high-resolution pattern. A pinhole of 0.5 mm in diameter was attached to the primary beam to limit the measurement area.
- **4.5. PL.** The intensity calibrated PL data have been acquired with a custom setup described elsewhere. The excitation has been carried out with 660 nm lasers coupled to homogenizer units. The excitation intensity was equivalent to >2 sun  $(6.1 \times 10^{21} \text{ photons m}^{-2} \text{ s}^{-1})$ . Relative PL measurements were carried out with a laser wavelength of 640 nm and an intensity equivalent to 1.22 W/cm<sup>2</sup>.
- **4.6. MOS Device Characterization.** Room-temperature CV measurements were carried out with an LCR meter from Agilent (E4990A) with an AC voltage of 30 mV at 25 °C.

## ASSOCIATED CONTENT

#### Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsami.1c02437.

XPS measurement of the absorber surface (Figure S1); comparison of the metal ratio values between XRF map

and EDX measurements (Figure S2); SEM cross section and PL measurement of Li- and Na-doped absorbers deposited on SLG (Figure S3); TOF-SIMS depth profile for the CZTSSe absorber on the rear structure SLG/Mo/Al $_2$ O $_3$  (Figure S4); and EDS maps for elements Cu, Zn, and Sn of CZTSSe absorbers (Figure S5) (PDF)

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The authors declare no competing financial interest.

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